

ME 323: FLUID MECHANICS-II

Dr. A.B.M. Toufique Hasan

Professor

Department of Mechanical Engineering

Bangladesh University of Engineering & Technology (BUET), Dhaka

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Choking Phenomena

toufiquehasan.buet.ac.bd toufiquehasan@me.buet.ac.bd



Consider, 1-D isentropic flow through a converging nozzle. A gas is expanded from a reservoir with thermodynamic conditions of p_0 and T_0 . The **back pressure** where the gas is **exhausted** is at static pressure of p_b .

The nozzle exit conditions are $M_{\rm e}$ and $p_{\rm e}$ (static).

- when $p_{\rm b} = p_0$; there will be no flow inside the nozzle.
- when $p_b < p_0$ (or $p_0 > p_b$); a flow will be induced from the reservoir and a jet with velocity M_e will be exhausted.
- The magnitude of jet Mach number (M_e) will be increased with the increase of pressure difference $(p_0 p_b)$.
- The reservoir senses the pressure at the exhaust (p_b) and induce the corresponding mass from the reservoir.
- So, mass flow rate will increase with increment of $(p_0 p_b)$.







Pressure distribution at difference back pressures (p_b)



Mass flow rate vs back pressure



cont...

- However, there is a limit upto which the mass flow rate will induce.
- •The mass flow rate will be the maximum (critical) when the Mach number at the nozzle exit is **sonic** i.e. $M_{\rm e} = 1.0$.

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- Further decrease in back pressure (p_b) will not result an increase in flow rate.
- The maximum mass flow rate, m_{max} will be occurred when $M_{\text{e}} = 1.0$.
- This is called the "choking" phenomena.
- upto choking condition, $p_{\rm e} = p_{\rm b}$





Once the flow reaches the sonic (critical) condition at throat (exit), it becomes "**deaf**" to downstream condition.

Any change (i.e. a reduction) in the applied back pressure (p_b) propagates in the fluid at the speed of sound in all directions, so it gets "**washed**" downstream by the fluid which is moving at the speed of sound at nozzle exit.

Jet cannot send any signal upstream to the reservoir (*or to influence the choked flow conditions*); consequently, **no more fluid is induced from the reservoir**.

For a fixed size of the throat, the maximum mass flow rate through the nozzle is determined by the choked condition.





cont.

The maximum possible mass flow rate is;

$$\dot{m}_{\max} = \rho^* A^* V^*$$

$$\Rightarrow \dot{m}_{\max} = \rho_0 \left(\frac{2}{k+1}\right)^{1/(k-1)} A^* \left(\frac{2k}{k+1} R T_0\right)^{1/2} \qquad \because V^* = M^* a^* = (1.0)\sqrt{kRT^*}$$

$$\Rightarrow \dot{m}_{\max} = \frac{p_0}{RT_0} \left(\frac{2}{k+1}\right)^{1/(k-1)} A^* \left(\frac{2k}{k+1} R T_0\right)^{1/2} \qquad \Rightarrow V^* = \sqrt{\frac{2k}{k+1} R T_0} \qquad ; \frac{T^*}{T_0} = \frac{2}{k+1}$$

$$\Rightarrow \dot{m}_{\max} = k^{1/2} \left(\frac{2}{k+1}\right)^{\frac{k+1}{2(k-1)}} A^* \frac{p_0}{\sqrt{RT_0}}$$

For air; k = 1.4 and R = 287 J/kgK:

$$\dot{m}_{\rm max} \approx 0.04 \; \frac{p_0 A^*}{\sqrt{T_0}} \qquad ({\rm kg/s})$$

For isentropic flow through a duct; the maximum mass flow possible is

cont...

- proportional to the throat area, A*
- proportional to stagnation pressure, p₀ and
- inversely proportional to the square root of the stagnation temperature, T_0 .

ṁ≠

 $\frac{\dot{m}}{\dot{m}_{max}}$

0

 $m_{\rm max}$

 p_b

 $\frac{P_b}{p_0}$

 $\dot{m} = f$

1.0

 $\frac{p^*}{p_0} = 0.528$



cont...

What will happen when

 $p_e > p_b \text{ (or } p_b < p_e)$

- Mass flow rate will not increase but will remain fixed as maximum as at choked condition.
- The exit jet will expand supersonically (M>1) outside the nozzle.
- The jet structure will be very complex with appearance of various waves (expansion and shocks).
- The condition is known as underexpansion.



Underexpanded jet



Underexpanded jet



Source: : Phys. Fluids 26, 096101 (2014) Int J Heat Fluid Flow (2013) 44: 140-154

cont...

Experimental Visualization through Schlieren Optical Imaging



$$T = \dot{m}V_e + (p_e - p_b)A_e$$

ideal underexpansion



Source: Behrouzi and McGuirk; AIAA J. (2015) DOI: 10.2514/1.J053376

cont.

Problem:

An Air cartridge is used to propel a small rocket cart. Compressed Air, stored at a pressure of 41.2 MPa (abs) and a temperature of 20°C, is expanded through a smoothly contoured converging nozzle with a throat area of 0.13 cm². Assume that the cartridge is well insulated and that the pressure surrounding the cartridge is 101 kPa (abs). For the given conditions,

- a. Calculate the pressure at the nozzle throat.
- b. Evaluate the mass flow rate of air through the nozzle.
- c. Determine the force, *F*, required to hold the cart stationary. (Assume frictionless roller)
- d. For what range of cartridge pressures will the flow through the nozzle be choked?



To be solved

(a) pe = 21.77 MPa
(b) 1.25 kg/s
(c) 673 N
(d) 191.2 kPa < pc < 41.2 MPa



Problem:

A convergent nozzle has an exit area of 6.25 cm². Air enters the nozzle with a stagnation pressure of 0.7 MPa and a stagnation temperature of 95°C. Determine the mass flow rate and jet exit velocity if it is discharging to an environment at (i) 0.6 MPa, (ii) 0.1 MPa, and (iii) 0 Pa.

Ans: (i) 0.66 kg/s ($p_b/p_0 = 0.857 > 0.528$ (not choked), $M_e = 0.47$, $p_e = 0.6MPa$, $V_e = 176.8$ m/s, $T_e = 352.4$ K, $\rho_e = 5.93$ kg/m³) (ii) 0.92 kg/s ($p_b/p_0 = 0.143 < 0.528$ (choked), $M_e = 1.0$, $p_e = 0.37MPa$, $V_e = 351$ m/s, $T_e = 306.5$ K, $\rho_e = 4.21$ kg/m³) (iii)



Problem

Air is being discharged to atmosphere ($p_b = 100 \text{ kPa}$) through a converging nozzle as shown in figure. The air is being feed from a large reservoir in which the pressure is continuously increased from 200 kPa to 600 kPa. During this operation, the reservoir temperature is maintained constant at 20°C.



(a) Complete the table:

po (kPa)	200	300	400	500	600
pe (kPa)					
Me					
<i>ṁ</i> (kg/s)					

(b) Plot \dot{m} vs. p_0



(c) Is the nozzle choked or not? Justify your comment.